

Advanced Output Coupling

Intercavity Doubling

$N_2:XXX$ may be a very popular gain medium, but it's the δH that's desired, not the fundamental.

(Not surprising. The optical noise is special.)

How do you set the δH ?

Eqs of motion for an electron:

$$F = ma$$

$$\ddot{x} = -\frac{eE(t)}{m} \quad \text{free electron}$$

In a medium, we'll have some damping force and the effect of the potential well:

$$\ddot{x} + \underbrace{\gamma \dot{x}}_{\text{damp}} + \underbrace{\omega_0^2 x}_{\text{harmonic potential well - linear restoring force}} + \underbrace{Ax^2 + Bx^3 + \dots}_{\text{anharmonic potential}} = -\frac{eE(t)}{m}$$

\nearrow $\omega \cos \omega t$

If the restoring force is linear: $x(t) = A \cos(\omega t + \phi)$

If not, x will have a more complicated form which must involve other frequencies

$P \equiv$ polarization $\propto x$



(Just giving a rough overview)

$$\vec{E}_in \rightarrow \vec{P} \rightarrow \vec{E}_{out}$$

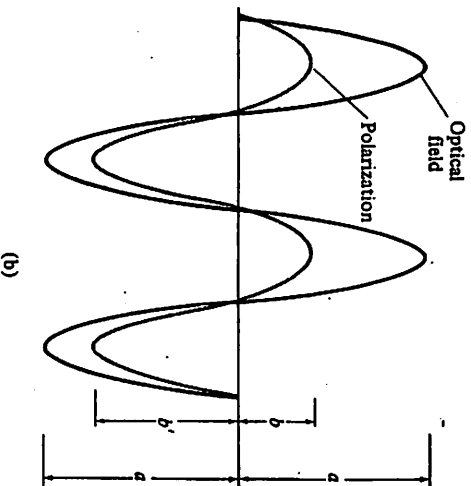
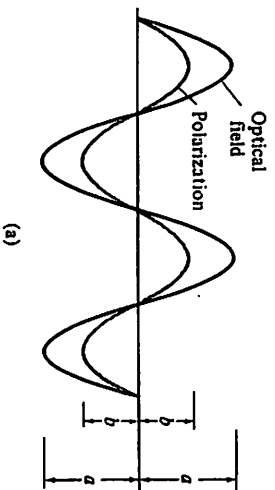


Figure 8-2 An applied sinusoidal electric field and the resulting polarization; (a) in a linear crystal and (b) in a crystal lacking inversion symmetry.

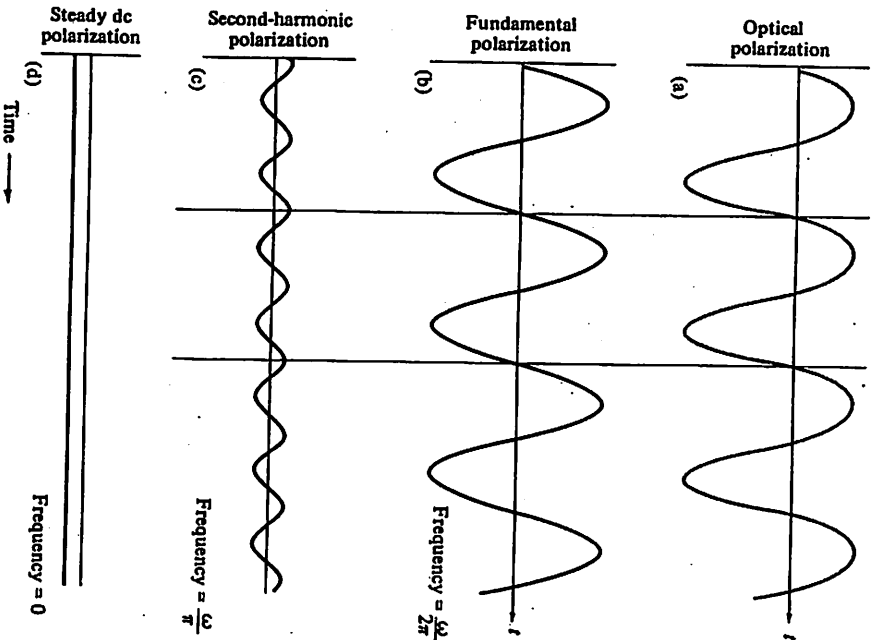


Figure 8-3 Analysis of the nonlinear polarization wave (a) of Figure 8.2(b) shows that it contains components oscillating at (b) the same frequency (ω) as the wave inducing it, (c) twice that frequency (2ω), and (d) an average (dc) negative component.

///

It's more convenient to express ρ in terms of ϵ :

$$\rho = \epsilon_0 \chi_1 E + \epsilon_0 \chi_2 E^2 + \epsilon_0 \chi_3 E^3 + \dots$$

$\underbrace{\quad}_{\omega} \quad \underbrace{\quad}_{\omega, \text{ zero}} \quad \underbrace{\quad}_{\omega^3, \omega}$

(No effort to use consistent notation here)

$$n = \sqrt{\epsilon} \approx \sqrt{\epsilon_0} \quad \epsilon = (1 + \chi_1) \epsilon_0$$

Recall: $\cos \omega_1 t \cos \omega_2 t = \frac{1}{2} [\cos(\omega_1 - \omega_2) + \cos(\omega_1 + \omega_2)]$

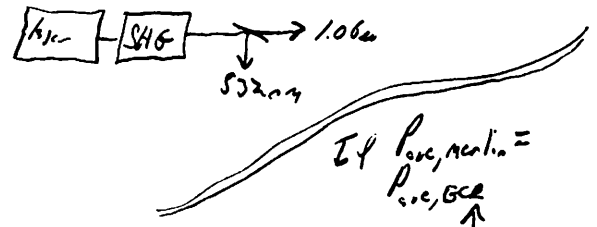
$$E_{out}^{2\omega} \propto \rho^{2\omega} \propto E^2 \propto I^{\omega}$$

$I^{2\omega} \propto (I^{\omega})^2 \Rightarrow$ You win big if the intensity is large

(Alternatively, you want a large E to explore the anisotropic regions of the potential.)

In general, this tends to mean you can't double ω on low energy pulsed beams

10 Hz Pulsed $\Rightarrow \approx \frac{1}{2} \text{ J/pulse} \quad 1.06 \mu\text{m}$
 (typical, 100-500 ns) $\approx \frac{1}{5} \text{ J/pulse} \quad 532 \text{ nm}$

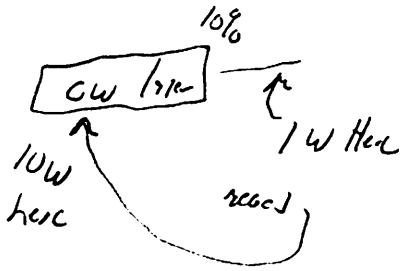


1 kHz Pulsed $\Rightarrow 1 \text{ MHz}, 200 \text{ ns}$ So, all other things being equal, the peak intensity is down by

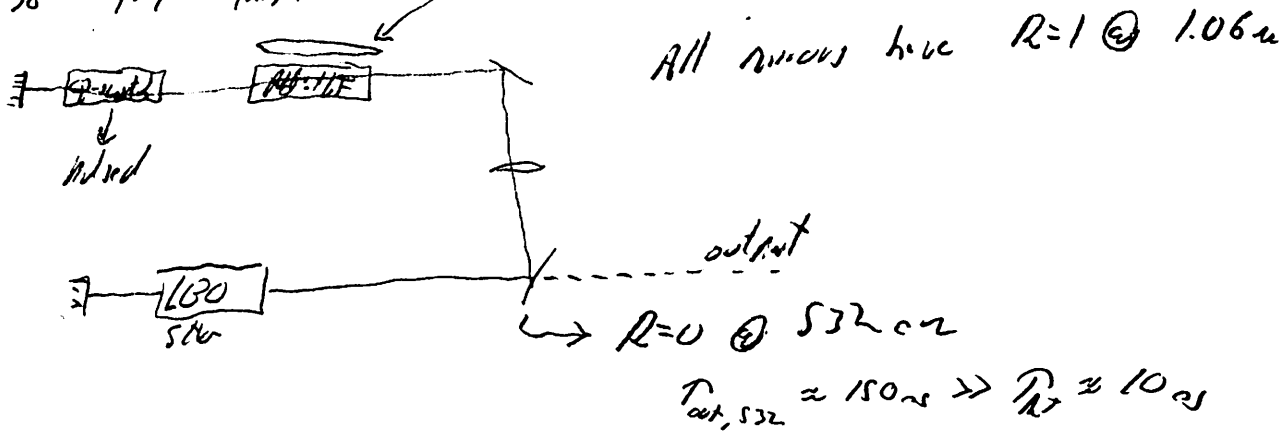
At $1.06 \mu\text{m} \Rightarrow \frac{I_{p,GR}}{I_{p,Merlin}} = \frac{20 \text{ Hz}}{1000 \text{ Hz}} \frac{S_{in}}{S_{out}} = \frac{1}{50} \frac{1}{20} = \frac{1}{1000}$

(If Merlin used an output coupler) So $I^{2\omega}$ will be down a lot!

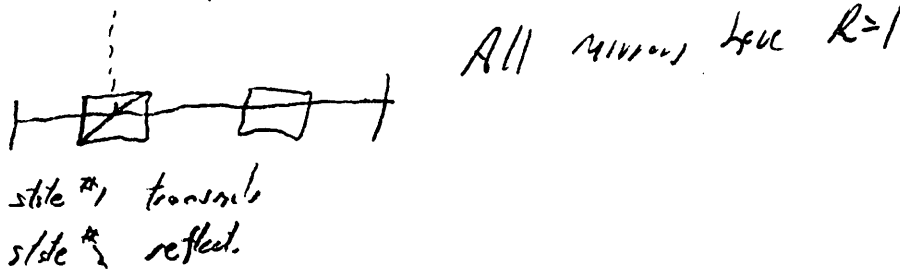
Put, set =



So for this. cw flash loss

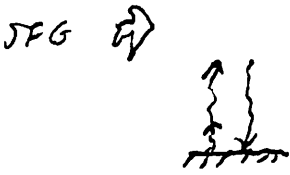
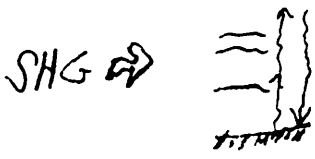


Coupling



Want increase the average power, right drop it.
Does increase the peak power compared to optimum output coupling case.

$$P_p = P_{AT} \text{ for CW pumping}$$



Photon splitting (optical parametric generation - OPG)
DFG



$$P^{(\omega)} = \chi_2 E^2 \quad E = E_0 (\cos \omega_1 t + \cos \omega_2 t)$$

$$\cos \omega_1 t + \cos \omega_2 t = \frac{1}{2} [\cos(\omega_1 - \omega_2)t + \cos(\omega_1 + \omega_2)t]$$

$$P^{(\omega)} \propto \chi_2 E_0^2 (\cos \omega_1 t + 2 \cos \omega_1 t \cos \omega_2 t + \cos \omega_2 t)$$

$$P^{(\omega)} = p^{(\omega)} + p^{2\omega_1} + p^{2\omega_2} + p^{(\omega_1 + \omega_2)} + p^{(\omega_1 - \omega_2)}$$

Only one of these will be phase matched

$\chi_1 \Rightarrow$ index of refraction

$\chi_2 \Rightarrow$ optical rectification. Pockels Effect
SHG, SFG, DFG, OPG

$\chi_3 \Rightarrow$ THG, ... \Rightarrow not so much important
Kerr effect

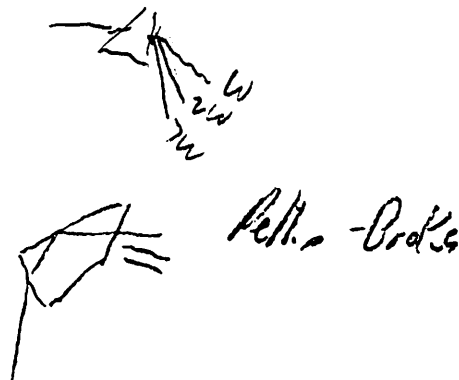
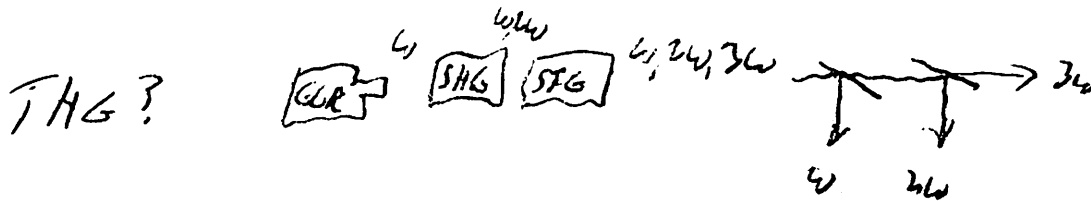
$$E = E_0 + E_{\omega} \cos \omega t$$

$$P^{(\omega)} = \epsilon_0 \chi^{(2)} E_0 E_{\omega} \cos \omega t$$

$$P = \epsilon_0 (\chi_1 + \chi^{(2)} E_0) E_{\omega} \cos \omega t \rightarrow n(E_0)$$

$$P = \epsilon_0 \chi E_{\omega} \cos \omega t \rightarrow n$$

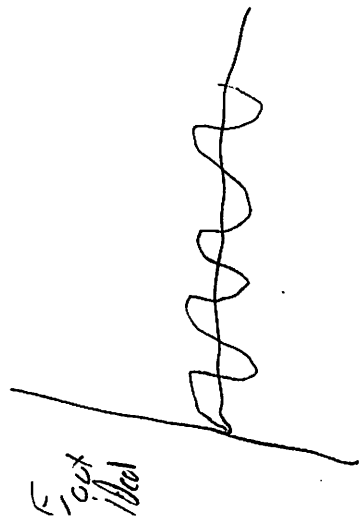
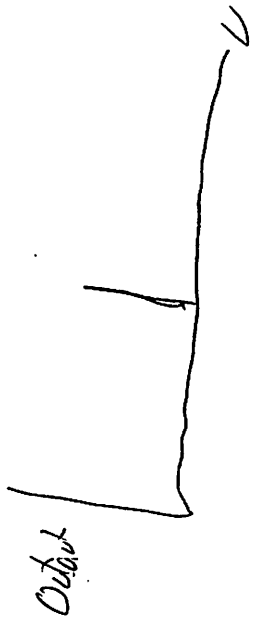
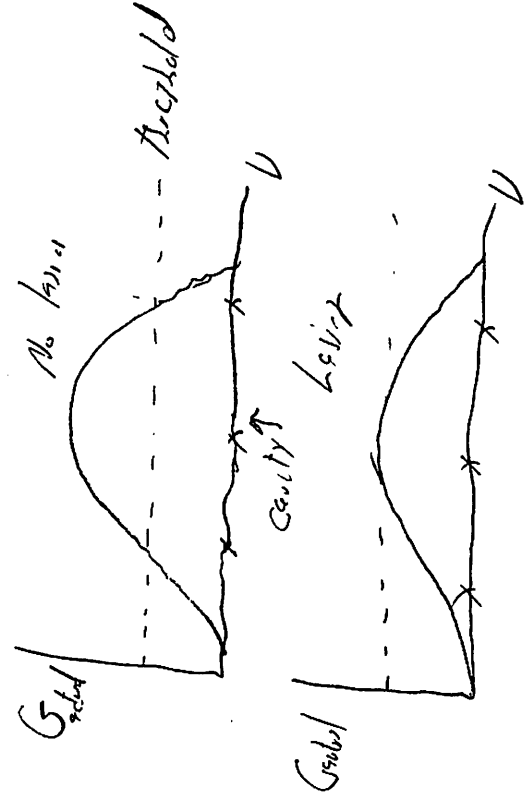
Pockels Effect



11/10/03

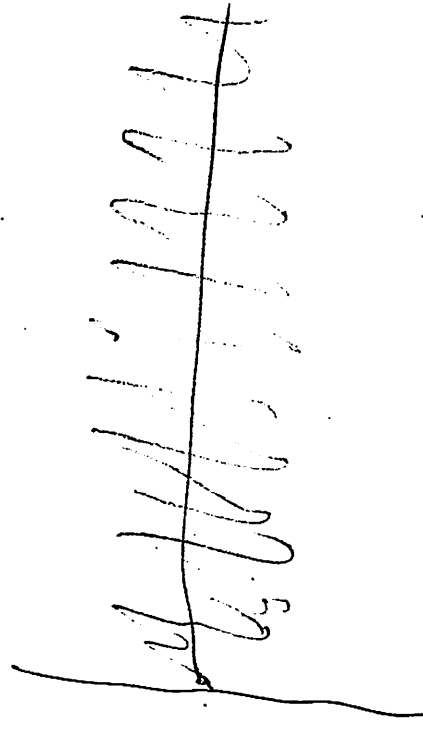
Output Spectrum

Homogeneous Broadening

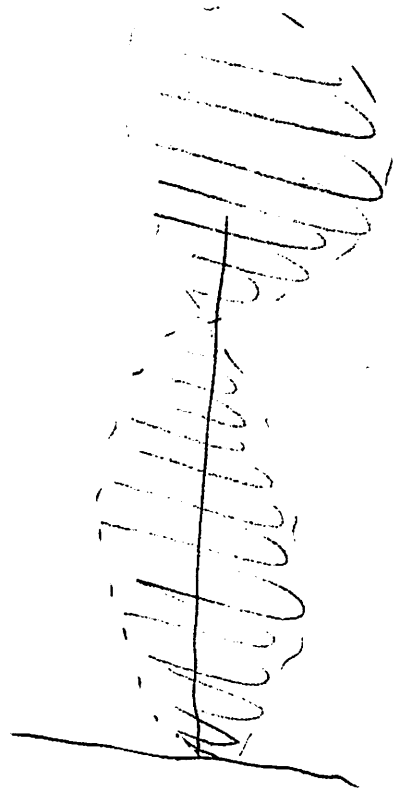
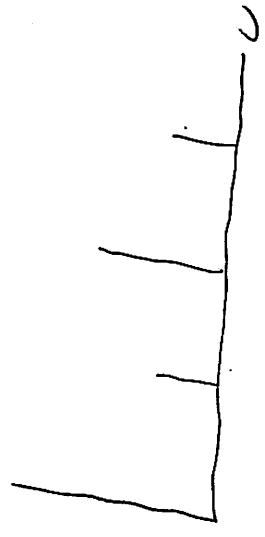
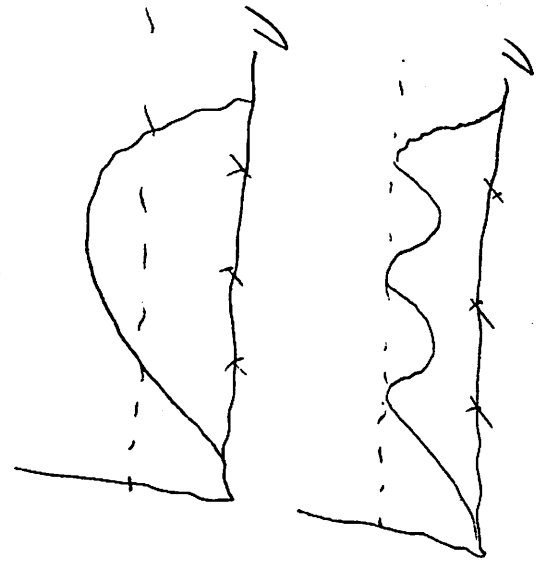


Exit Ideal

Exit Ideal



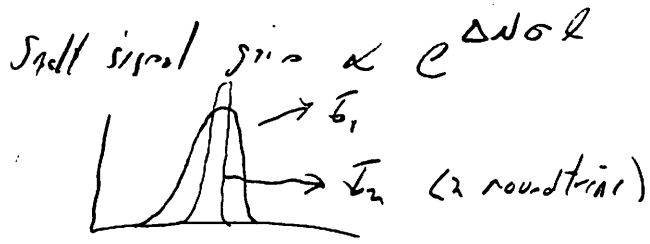
Inhomogeneous



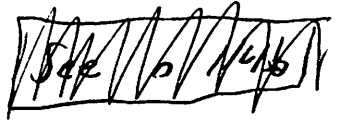
It can't be made better the number

Line width

→ roughly a measure of the cross-section (even if the overall linewidth is small)

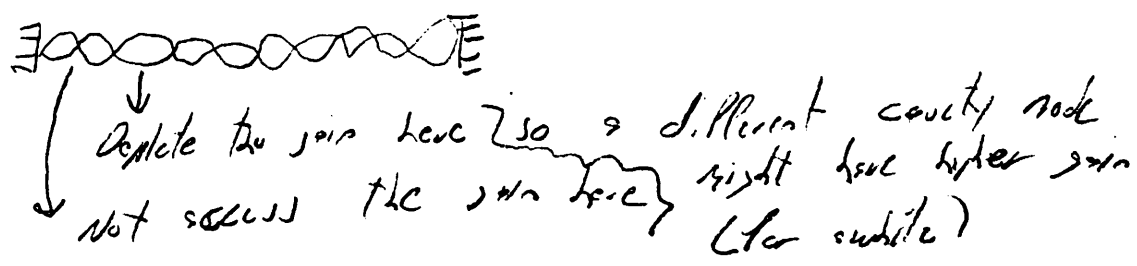


Gain narrowing. (Homogeneously broadened case)

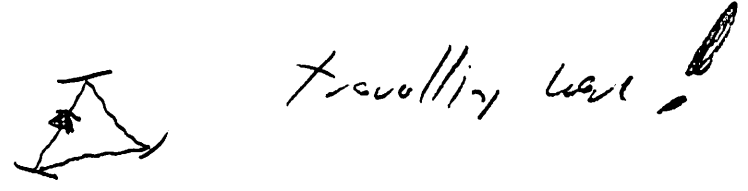


The next step might be to go to a single cavity mode.
 Invert line width narrowing effects.
 Make the cavity short. (Diode laser cavities can be very short!)

There's a problem however in longer cavities →



One solution to this is to go to a ring cavity with an optical diode.



Model calculation for a single mode HeNe (γ_{1114} , QE)

$\Delta\nu_{1/2}$ is the width of the cavity resonance.

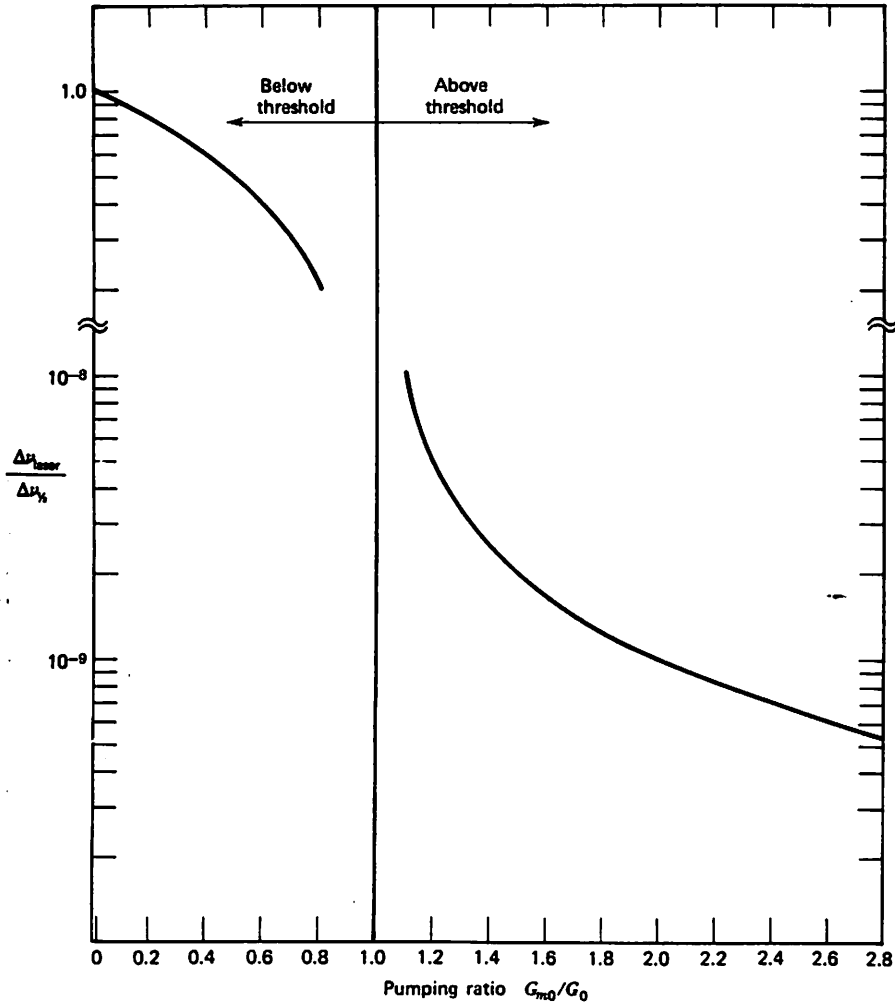
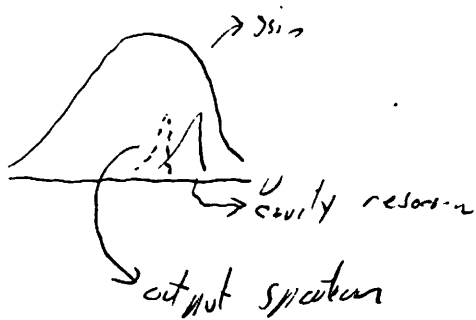


FIGURE 21.5 The laser mode linewidth below threshold [Eq. (21.2-15)] and above threshold [Eq. (21.2-19)]. The data used in the plot correspond to the He-Ne laser example of Section 21.2. Note the break in the ordinate scale.

Frequency Pulling

Things are a little more complicated



For a homogeneous broadband system

$$\nu = \frac{\nu_0}{\Delta\nu_0} + \frac{\nu_c}{\Delta\nu_c}$$

$$\frac{1}{\Delta\nu_0} + \frac{1}{\Delta\nu_c}$$

You'll need this in the next HW assignment

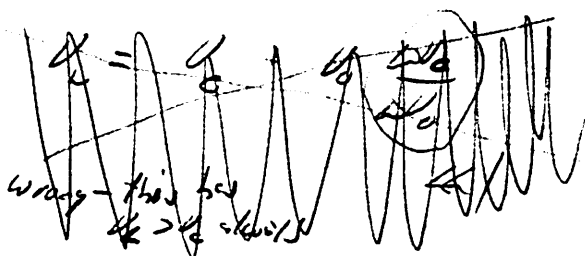
transition resonance and width

$$\nu = \frac{\nu_0}{\Delta\nu_0} + \frac{\nu_c}{\Delta\nu_c} \approx \left(\nu_0 \frac{\Delta\nu_c}{\Delta\nu_0} + \nu_c \right) \left(1 - \frac{\Delta\nu_c}{\Delta\nu_0} \right)$$

$$\frac{1}{\Delta\nu_c} \left(\frac{\Delta\nu_c}{\Delta\nu_0} + 1 \right)$$

$$\approx \nu_c + (\nu_0 - \nu_c) \frac{\Delta\nu_c}{\Delta\nu_0}$$

If $\Delta\nu_0 \gg \Delta\nu_c$, the gain spectrum is broad and constant



The slope is can be a decent approx. for inhom. systems depends on circumstances

$\Delta\nu_0 \approx 300 \text{ GHz}$ for solid state rubic

$\Delta\nu_c \approx 10 \text{ MHz}$ for

low loss, ultra-irred cavity

What limits $\Delta\nu_c$?

$$\nu_c = N \frac{c}{2L_{opt}}$$

$$\frac{d\nu_c}{dL_{opt}} = -N \frac{c}{2L_{opt}^2} = \left(\frac{Nc}{2L_{opt}} \right) \left(-\frac{1}{L_{opt}} \right)$$

(Assuming N doesn't change!)

$$\frac{\Delta\nu_c}{\nu_c} \approx \frac{\Delta L_{opt}}{L_{opt}}$$

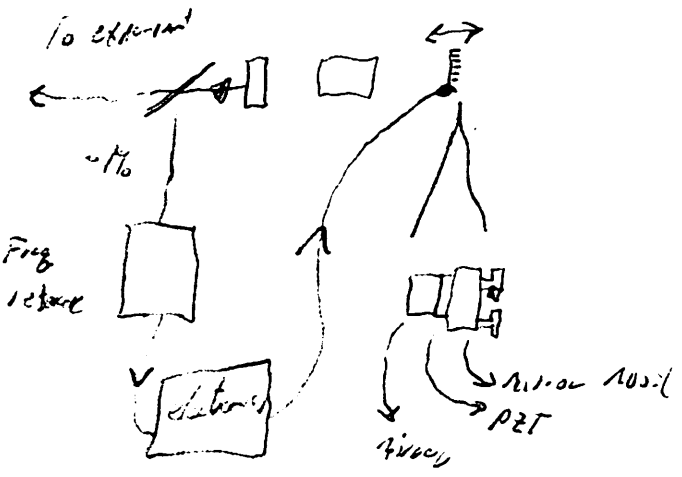
and L_{opt} can change due to thermal fluctuations, gain fluctuations, mirror movement

For a 1m cavity, $\lambda = 532 \text{ nm}$, $\Delta\nu_0 = 10 \text{ MHz} \Rightarrow \Delta L_{opt} \approx 200 \text{ nm}$ ✓

see your E
eqs 9.1-21
and preceding
derivations

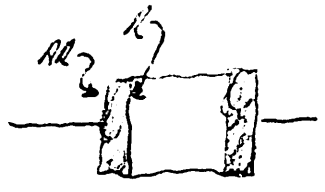
117
114E

Not surprisingly, then, active stabilization is often used in critical applications



(PZT effect is related to SFG!)

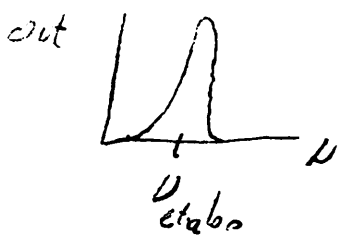
Freq. reference



air space etalon

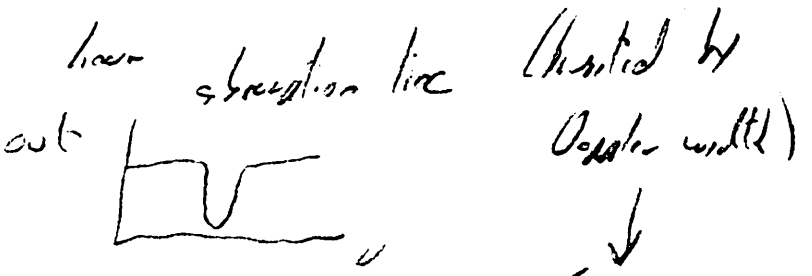
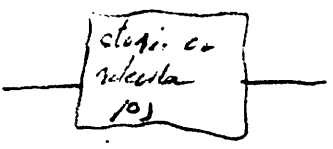
"Fabry-Pérot" etalon

- temp stabilized
- enclosed
- control servos



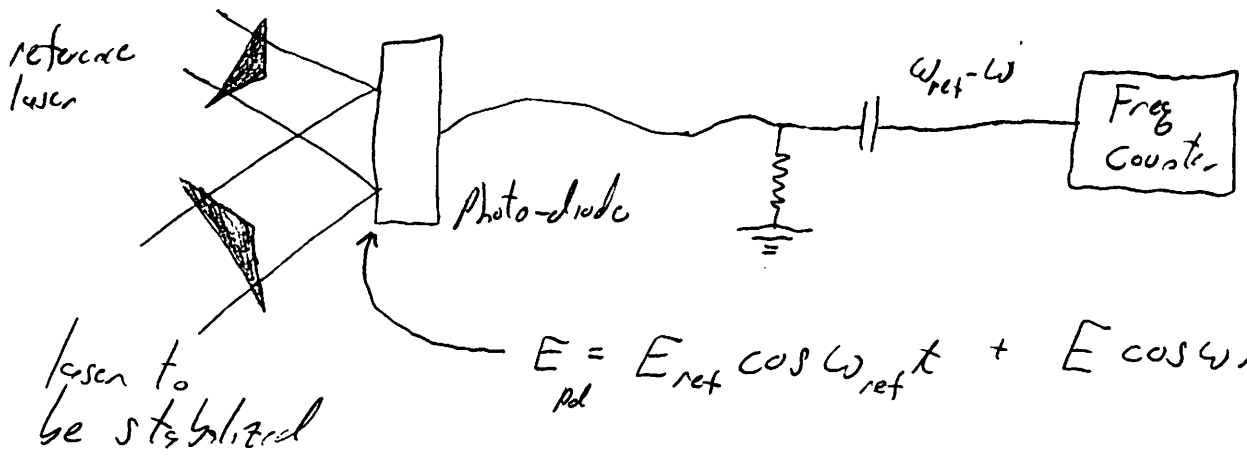
can be whatever you want

- Careful, don't let intensity fluctuations fool you.
- The most obvious ways to use the signal are...



There are non-linear spectrometric techniques that can do this

Once you have a stable laser operating at a single narrow line, you can use it to stabilize other lasers sometimes.



$$E_{pd} = E_{ref} \cos \omega_{ref} t + E \cos \omega t$$

This will work if $|\omega_{ref} - \omega| \approx \text{GHz}$.

However, a new technique has been developed* that, in principle, allows you to measure (and hence stabilize) a laser operating anywhere in or near the optical spectrum.

Amazingly, the heart of the system is a short pulse laser which necessarily has a broad linewidth:

$$\Delta \nu \tau \approx 1$$

For $\tau = 50 \text{ fs}$, $\Delta \nu \approx 2 \cdot 10^{13} \text{ Hz}$.

IP $\lambda = 800 \text{ nm}$, $\Delta \lambda / \lambda = 5\%$!

* See the class web page for a reference.

Q-switching (Text section 8.4)

Q-switching involves switching the cavity Q from an initially low value (high loss) to a high value (low loss).

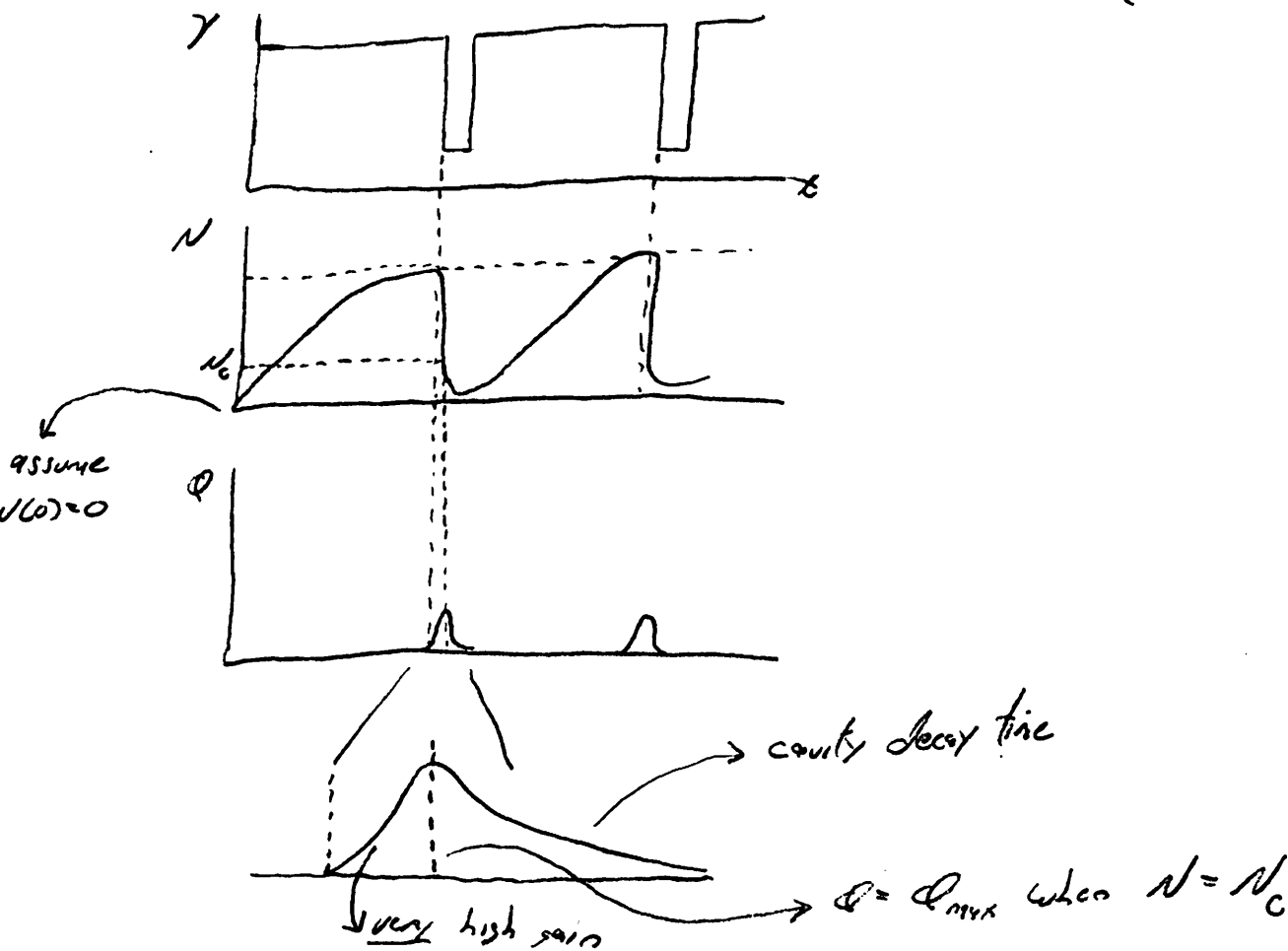
It can allow the generation of high energy pulses with pulse width on order τ_{RT} .

Recall, for CW pumping and no Q-switching:

$$\left. \begin{aligned} N_0 &= N_c = \frac{\gamma}{\sigma L} \\ Q_0 &= V_c \tau_c [R_p - N_0/\rho] \end{aligned} \right\} \text{after steady-state is reached.}$$

If you Q-switch w/ CW pumping:

$$\left\{ \begin{aligned} \frac{dN}{dt} &= R_p - N/\tau \\ N_0 &= R_p \tau \end{aligned} \right.$$



• This does not allow you to more efficiently use your pump source \Rightarrow this is not a way to increase P_{ave}

if $P_{cw} = 10W = 10 J/s$
 $E_{pulse, 10Hz} = 1J$ $P = \frac{1J}{10ns} = 10^8 W$

• Because we can have $N \gg N_c$, this does allow fast extraction of energy \Rightarrow giant pulses

• Once you reach N_{max} you should Q-switch, otherwise you reduce the rep. rate and P_{ave} available.

if 1 kHz rep rate:
 $\tau = 200ns$ $P_{cw} = 10W = 10 J/s \Rightarrow E_{pulse} \leq 10 \mu J$ $P \approx \frac{10 \mu J}{100ns} = 10^5 W$

• Often the pump is pulsed. You want $\tau_{pump} \ll \tau$ or you waste pump power.

$$\dot{N}_2 = R - \frac{N_2}{\tau} = 0$$

$$N_{2, steady state} = R\tau$$

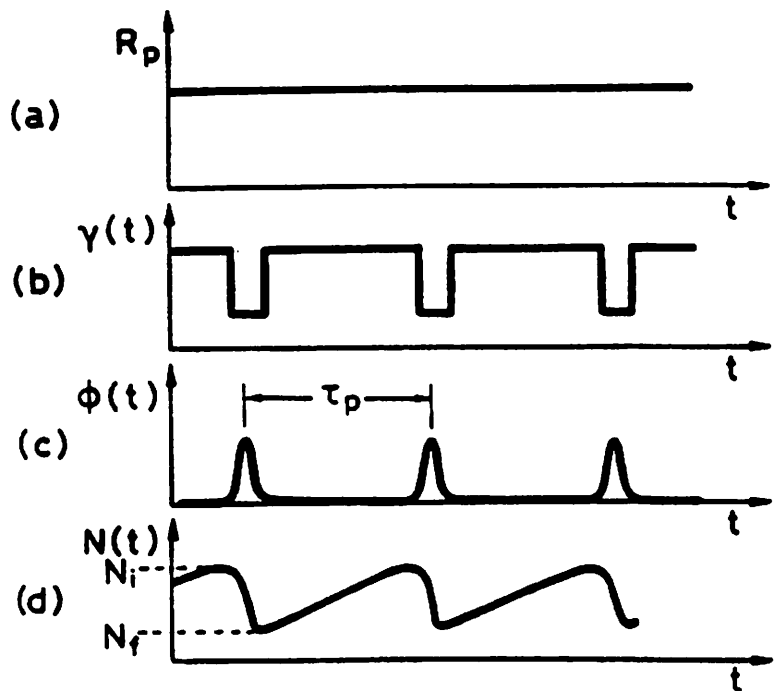
★ Q-switching is usually reserved for media with $\tau \approx 100 \mu s$ and above (Nd:xxx, but not He:Ne, Ar⁺).

• CW-pumped: max rep rate $\approx \frac{1}{\tau} \approx kHz$
(limited by time to reach N_{max})

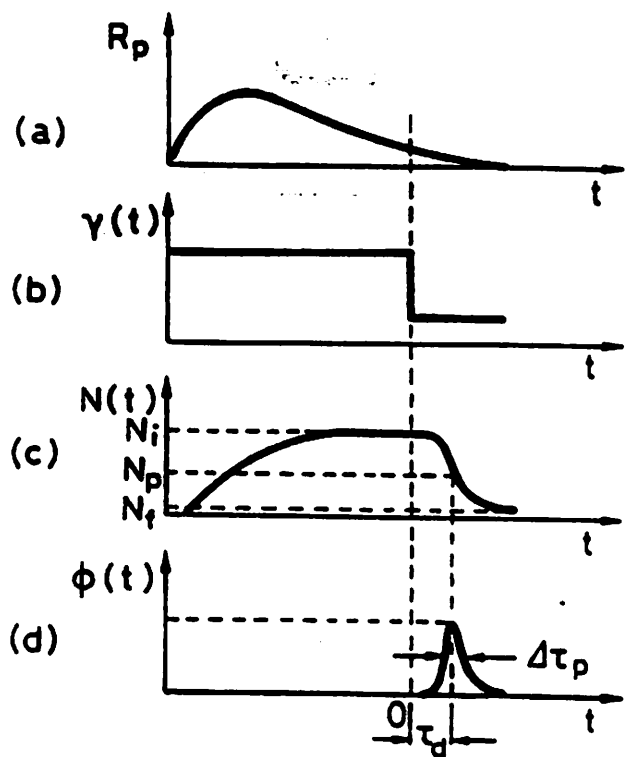
pulsed-pumped max rep rate $\approx Hz$
(limited by flash lamps, heating of gain medium)

• Mode competition can be less effective.
Injection!

• In all this, we assume $\tau_{switch} \ll \tau_c$



CW pumped
(Fig 8.10)

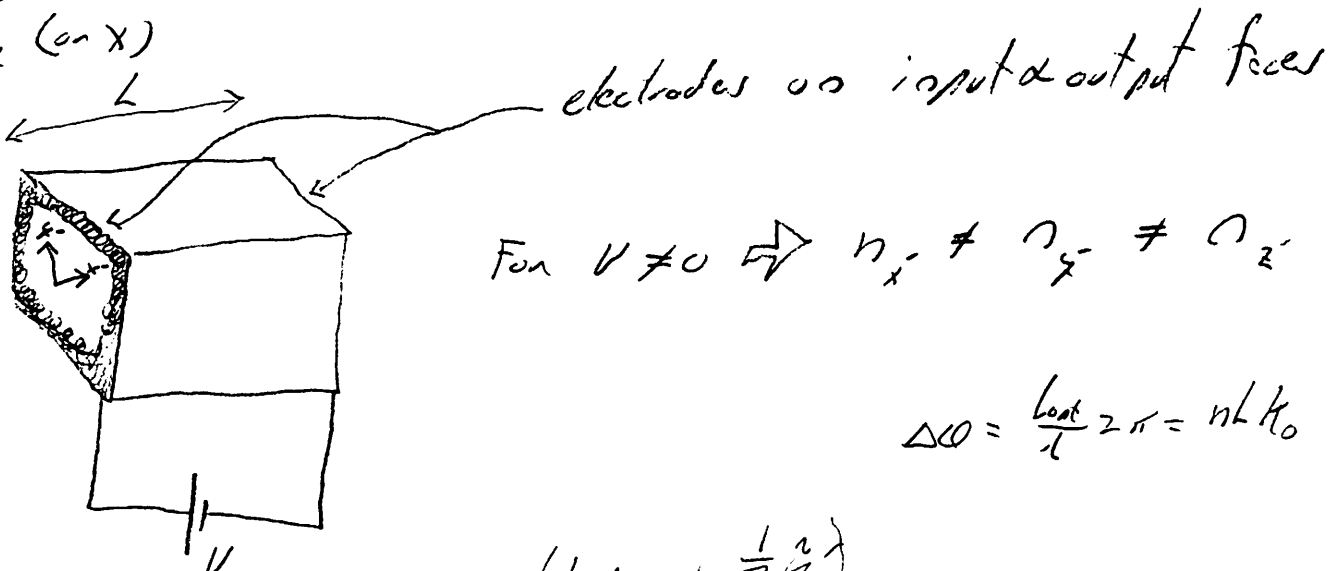
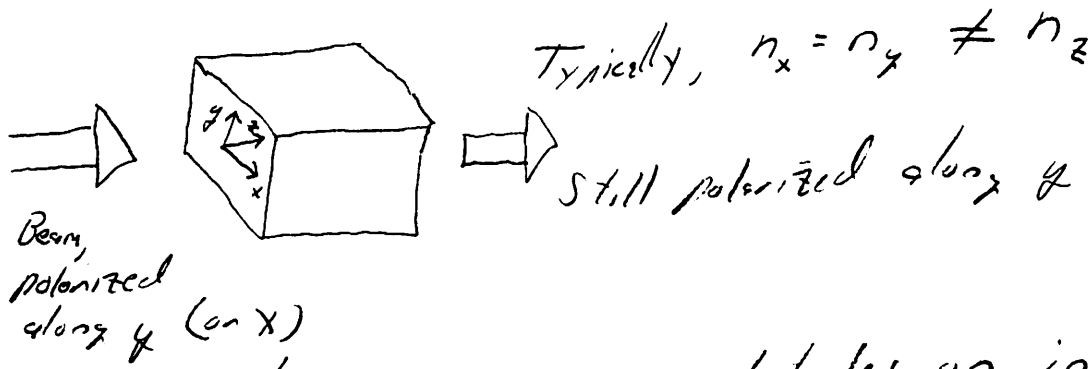


Pulsed pump
(Fig 8.9)

Most common methods use the electro-optic or acousto-optic effects.

Electro-optic switching

Uses the response of an anisotropic crystal to an electric field \Rightarrow Pockels Effect



For $V \neq 0 \Rightarrow n_x \neq n_y \neq n_z$

$$\Delta \phi = \frac{k_0 L}{\lambda} 2\pi = n L k_0$$

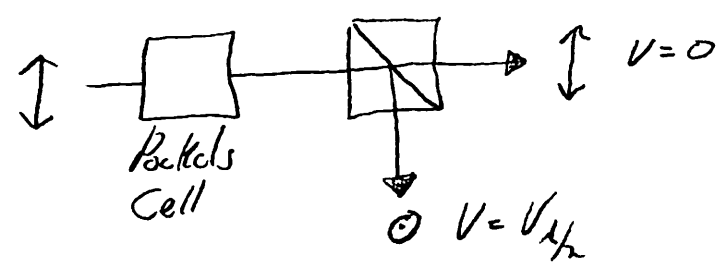
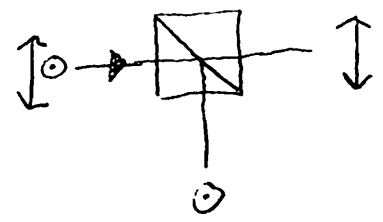
Suppose, initially: $\vec{E}_i = \hat{E}_0 \hat{y} = E_0 \left(\frac{1}{\sqrt{2}} \hat{x}' + \frac{1}{\sqrt{2}} \hat{z}' \right)$
 At the output face: $\vec{E}_s = E_0 \left(\frac{1}{\sqrt{2}} \hat{x}' e^{i k_0 n_x L} + \frac{1}{\sqrt{2}} \hat{z}' e^{i k_0 n_z L} \right)$

$$= \frac{E_0}{\sqrt{2}} \left(\hat{x}' + \hat{z}' e^{-i \phi(V)} \right) e^{i k_0 n_y L} \quad \left\{ \begin{array}{l} \phi = k_0 L (n_z - n_x) \\ \text{or} \\ \phi = \Delta \phi \end{array} \right.$$

Select $V = V_{\pi/2}$ meaning $\phi = \pi$.

$$\vec{E}_s = \frac{E_0}{\sqrt{2}} (\hat{x}' - \hat{z}') e^{i \phi_0} = \underline{\underline{E_0 \hat{x}' e^{i \phi_0}}}$$

Suppose we add a polarizer



Typically, $V_{\lambda/4} \approx 5000V$

Actually, in a laser cavity, you are more likely to see this:



and using $V = V_{\lambda/4}$.

Advantages

- Fast switching times
- Capable of very high and low loss ($\sim 99\% + \sim 2\%$)
- Can be scaled to large diameter - suitable for high power

Disadvantage

- low rep. rate.

Acousto-optic switching

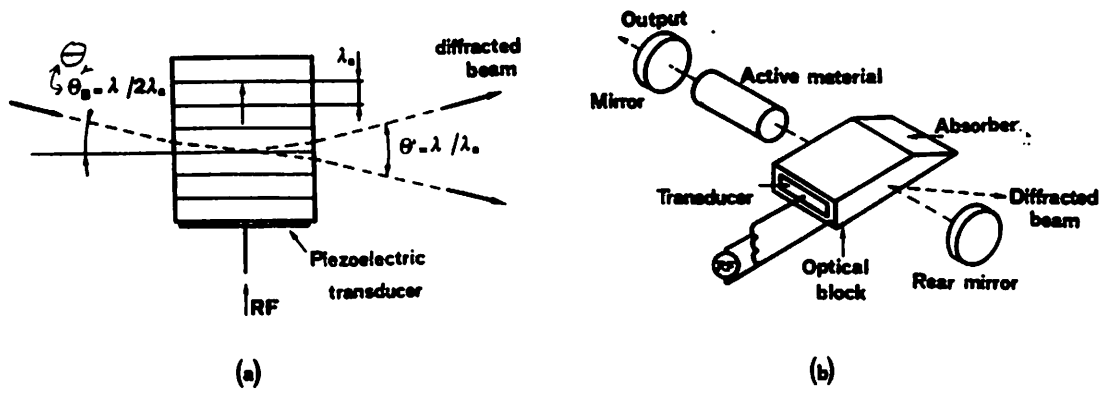
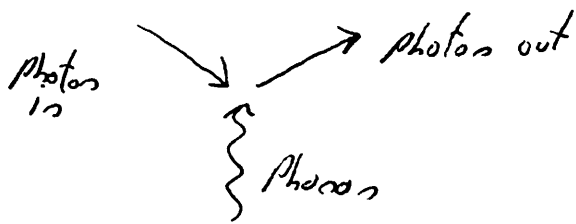


FIG. 8.7. (a) Incident, transmitted, and diffracted beams in an acousto-optic modulator (Bragg regime). (b) Q-switched laser arrangement incorporating an acousto-optic modulator.



$$h\nu_{out} = h\nu_{in} + E_{photon}$$

so this is a way to change the frequency a little

Advantages

- Rep. rate by ability to modulate RF \Rightarrow much faster than 1/f
- Low insertion loss

Disadvantages

- Maximum loss is modest
- Large apertures are possible, but harder